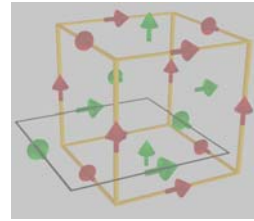




FDTD Method

$$\begin{aligned}\mu \frac{\partial \vec{H}}{\partial t} &= -\nabla \times \vec{E} \\ \epsilon \frac{\partial \vec{E}}{\partial t} &= \nabla \times \vec{H} - \vec{J}\end{aligned}$$



Outline

- **Basics**
 - Maxwell's Equations
 - Spatial discretisation/Time discretisation
 - Equivalent Circuit for FDTD
 - Stability
 - Ports
- **Simple Examples**
- **Accuracy and Losses**
- **Speedups on modern Computers**
- **Conclusions**

Maxwell's Equations



Parameters

$$\mu \frac{\partial \vec{H}}{\partial t} = -\nabla \times \vec{E}$$
$$\epsilon \frac{\partial \vec{E}}{\partial t} = \nabla \times \vec{H} - \vec{J}$$

Electric Field

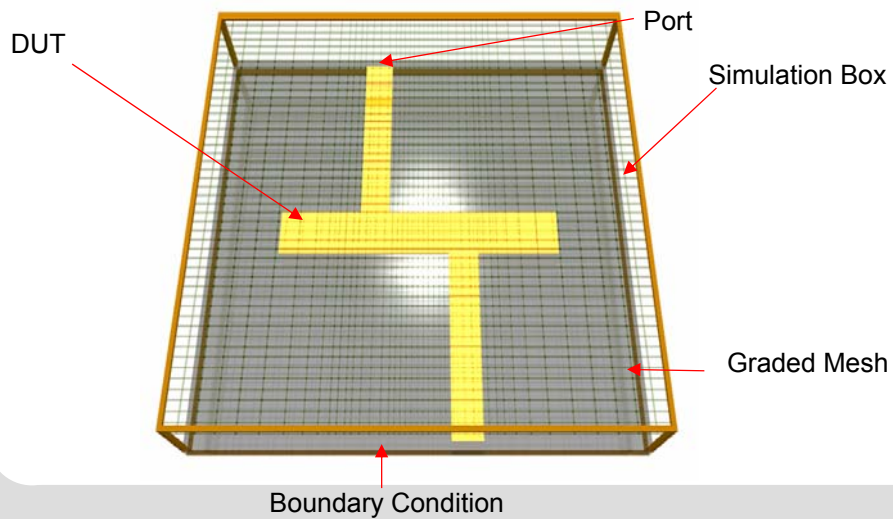
Magnetic Field

Excitation

- Hyperbolic partial differential equation, initial boundary value problem
- Time domain tracking of the electromagnetic field
- Passive component analysis



Spatial FDTD Principle



FDTD Basics



Maxwell's Equations

$$\mu \frac{\partial \vec{H}}{\partial t} = -\nabla \times \vec{E}$$

$$\varepsilon \frac{\partial \vec{E}}{\partial t} = \nabla \times \vec{H} - \vec{J}$$

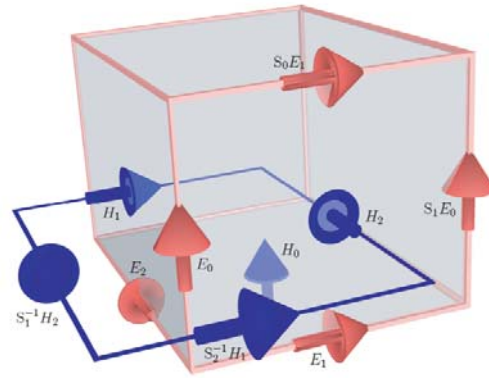


Spatial discretization

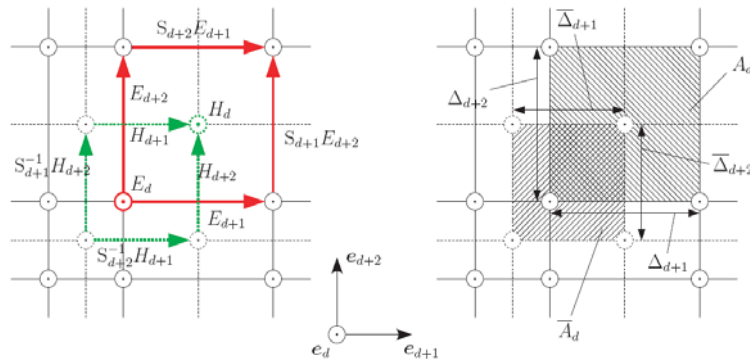
$$\mu \frac{\partial \vec{H}}{\partial t} = -\frac{1}{\Delta_x} \sum_{\odot} \vec{E}$$

$$\varepsilon \frac{\partial \vec{E}}{\partial t} = \frac{1}{\Delta_x} \sum_{\odot} \vec{H} - \vec{J}$$

Yee cell



Spatial Discretisation



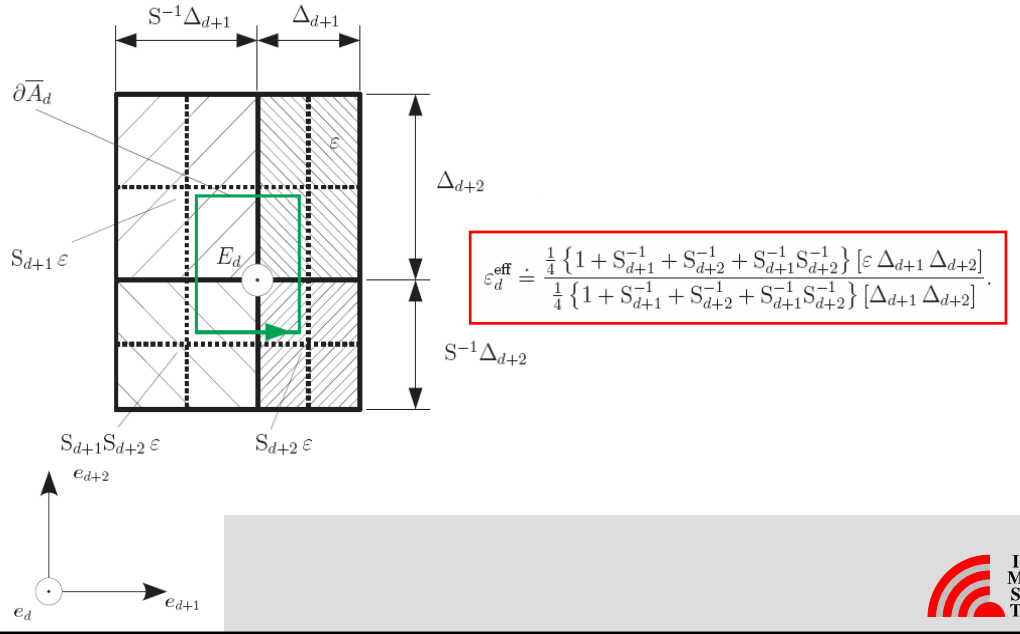
$$\oint_{\partial \bar{A}_d} \mathbf{H} \cdot d\ell \approx \{1 - S_{d+1}^{-1}\} H_{d+2} \bar{\Delta}_{d+2} - \{1 - S_{d+2}^{-1}\} H_{d+1} \bar{\Delta}_{d+1} =$$

$$+ \left(\varepsilon_d^{\text{eff}} \frac{d}{dt} E_d + \kappa_d^{\text{eff}} E_d - J_d^{\text{src}} \right) \bar{\Delta}_{d+1} \bar{\Delta}_{d+2} \approx \iint_{\bar{A}_d} \dots \cdot dA,$$

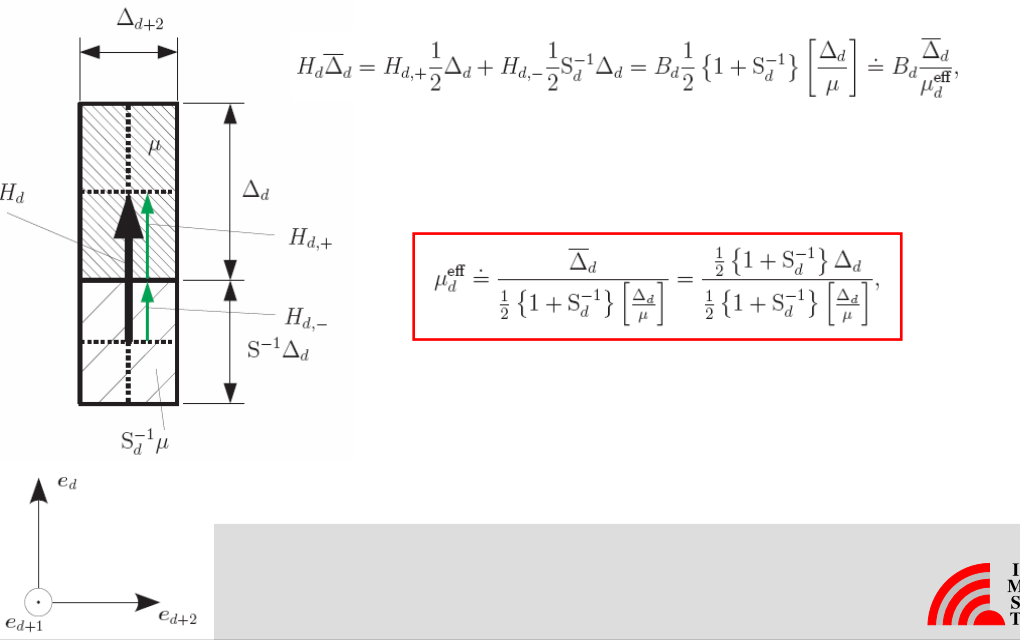
$$\oint_{\partial A_d} \mathbf{E} \cdot d\ell \approx \{S_{d+1} - 1\} E_{d+2} \Delta_{d+2} - \{S_{d+2} - 1\} E_{d+1} \Delta_{d+1} =$$

$$- \left(\mu_d^{\text{eff}} \frac{d}{dt} H_d + \sigma_d^{\text{eff}} H_d \right) \Delta_{d+1} \Delta_{d+2} \approx \iint_{A_d} \dots \cdot dA.$$

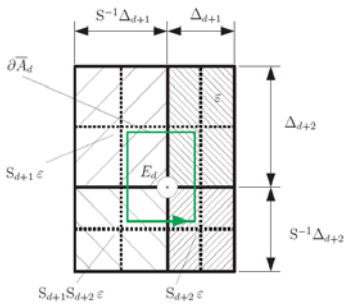
Effective Electric Materials



Effective Magnetic Materials



Electric Equivalent Circuit Elements



$$\{1 - S_{d+1}^{-1}\} H_{d+2} \bar{\Delta}_{d+2} - \{1 - S_{d+2}^{-1}\} H_{d+1} \bar{\Delta}_{d+1} = -\bar{\Delta}_{d+1} \bar{\Delta}_{d+2} J_d^{\text{src}}$$

$$+ \frac{1}{4} \{1 + S_{d+1}^{-1} + S_{d+2}^{-1} + S_{d+1}^{-1} S_{d+2}^{-1}\} [\varepsilon \Delta_{d+1} \Delta_{d+2}] \frac{1}{\Delta_d} \frac{d}{dt} E_d \Delta_d$$

$$+ \frac{1}{4} \{1 + S_{d+1}^{-1} + S_{d+2}^{-1} + S_{d+1}^{-1} S_{d+2}^{-1}\} [\kappa \Delta_{d+1} \Delta_{d+2}] \frac{1}{\Delta_d} E_d \Delta_d,$$

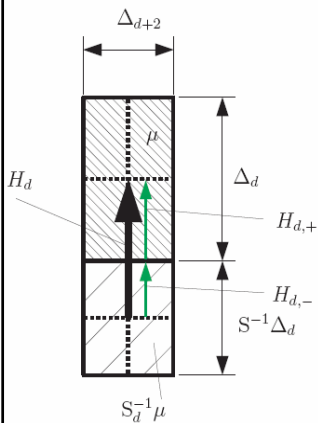
$$E_d \Delta_d \doteq v_d \quad \downarrow \quad H_d \bar{\Delta}_d \doteq i_d$$

$$\{1 - S_{d+1}^{-1}\} i_{d+2} - \{1 - S_{d+2}^{-1}\} i_{d+1} + i_{\text{src},d} = C_d \frac{d}{dt} v_d + G_d v_d,$$

➤ Kirchhoffsche Knotenregel



Magnetic Equivalent Circuit Elements



$$\{S_{d+1} - 1\} E_{d+2} \Delta_{d+2} - \{S_{d+2} - 1\} E_{d+1} \Delta_{d+1} =$$

$$-\frac{\Delta_{d+1} \Delta_{d+2}}{\frac{1}{2} \{1 + S_d^{-1}\} \left[\frac{\Delta_d}{\mu} \right]} \frac{d}{dt} H_d \bar{\Delta}_d + \frac{\Delta_{d+1} \Delta_{d+2}}{\frac{1}{2} \{1 + S_d^{-1}\} \left[\frac{\Delta_d}{\sigma} \right]} H_d \bar{\Delta}_d.$$

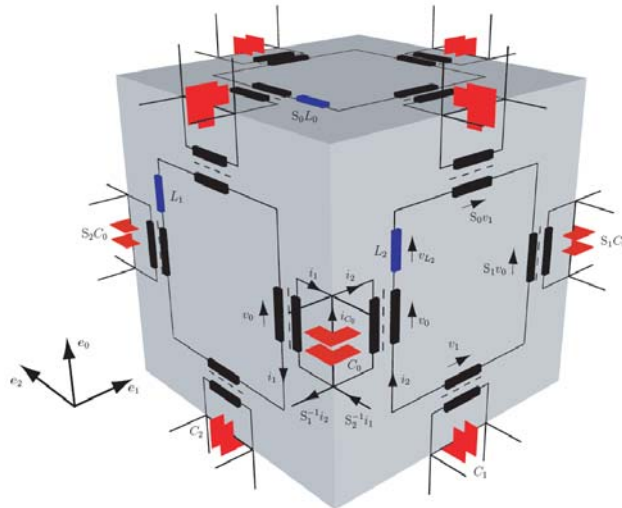
$$E_d \Delta_d \doteq v_d \quad \downarrow \quad H_d \bar{\Delta}_d \doteq i_d$$

$$\{S_{d+1} - 1\} v_{d+2} - \{S_{d+2} - 1\} v_{d+1} = -L_d \frac{d}{dt} i_d - R_d i_d,$$

➤ Kirchhoffsche Maschenregel



3D Equivalent Circuit for FDTD Method



$$\{1 - S_{d+1}^{-1}\} i_{d+2} - \{1 - S_{d+2}^{-1}\} i_{d+1} + i_{src,d} = + C_d \frac{d}{dt} v_d + G_d v_d,$$

$$\{S_{d+1} - 1\} v_{d+2} - \{S_{d+2} - 1\} v_{d+1} = - L_d \frac{d}{dt} i_d - R_d i_d,$$

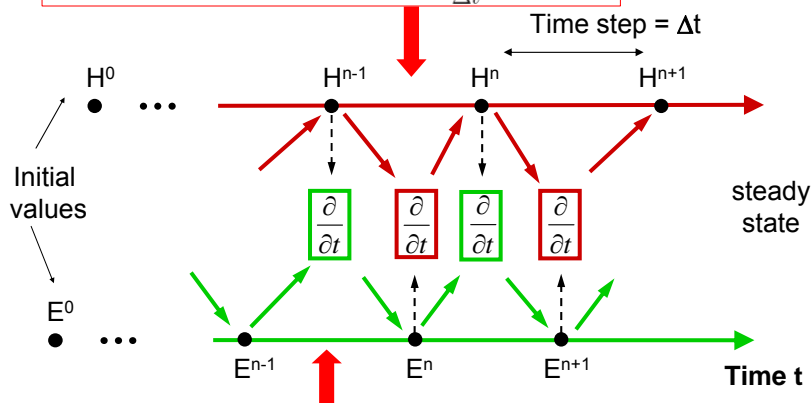


Nov-07 © IMST GmbH - All rights reserved

Time Discretisation



$$\{S_{d+1} - 1\} v_{d+2} - \{S_{d+2} - 1\} v_{d+1} = - \frac{L_d}{\Delta t} \{1 - S_t^{-1}\} i_d$$



$$\{1 - S_{d+1}^{-1}\} S_t^{-1} i_{d+2} - \{1 - S_{d+2}^{-1}\} S_t^{-1} i_{d+1} + S_t^{-1} i_{src,d} = + \frac{C_d}{\Delta t} \{1 - S_t^{-1}\} v_d$$

- Time domain tracking of EM field
- Fourier transformation after steady state

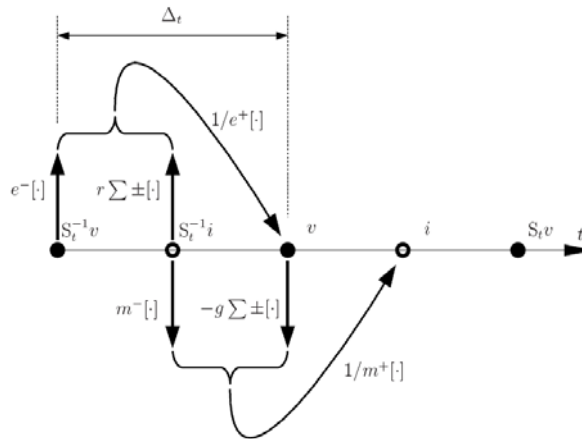


Nov-07 © IMST GmbH - All rights reserved

Time Iteration

$$v_d = \frac{e_d^- S_t^{-1} v_d + r_d (\{1 - S_{d+1}^{-1}\} S_t^{-1} i_{d+2} - \{1 - S_{d+2}^{-1}\} S_t^{-1} i_{d+1} + S_t^{-1} i_{\text{src},d})}{e_d^+},$$

$$i_d = \frac{m_d^- S_t^{-1} i_d - g_d (\{S_{d+1} - 1\} v_{d+2} - \{S_{d+2} - 1\} v_{d+1})}{m_d^+},$$



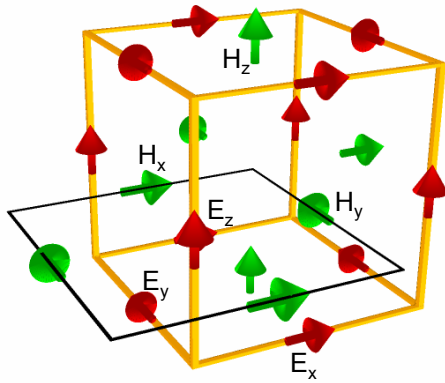
Stability (1)

Time Step limited by **spatial resolution**

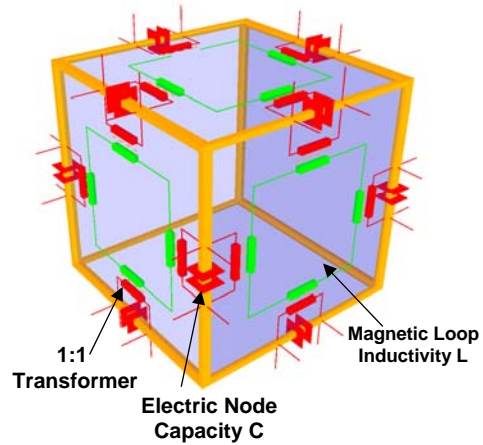
$$\Delta_t \leq \min \left[\frac{\sqrt{\epsilon_r}}{c_0} \cdot \frac{1}{\sqrt{\left(\frac{1}{\Delta x}\right)^2 + \left(\frac{1}{\Delta y}\right)^2 + \left(\frac{1}{\Delta z}\right)^2}} \right]$$

- Classical FDTD stability criterion
- Small details: long simulation time

FDTD Equivalent circuit



Equivalent Circuit



Nov-07 © IMST GmbH - All rights reserved



Stability (2)



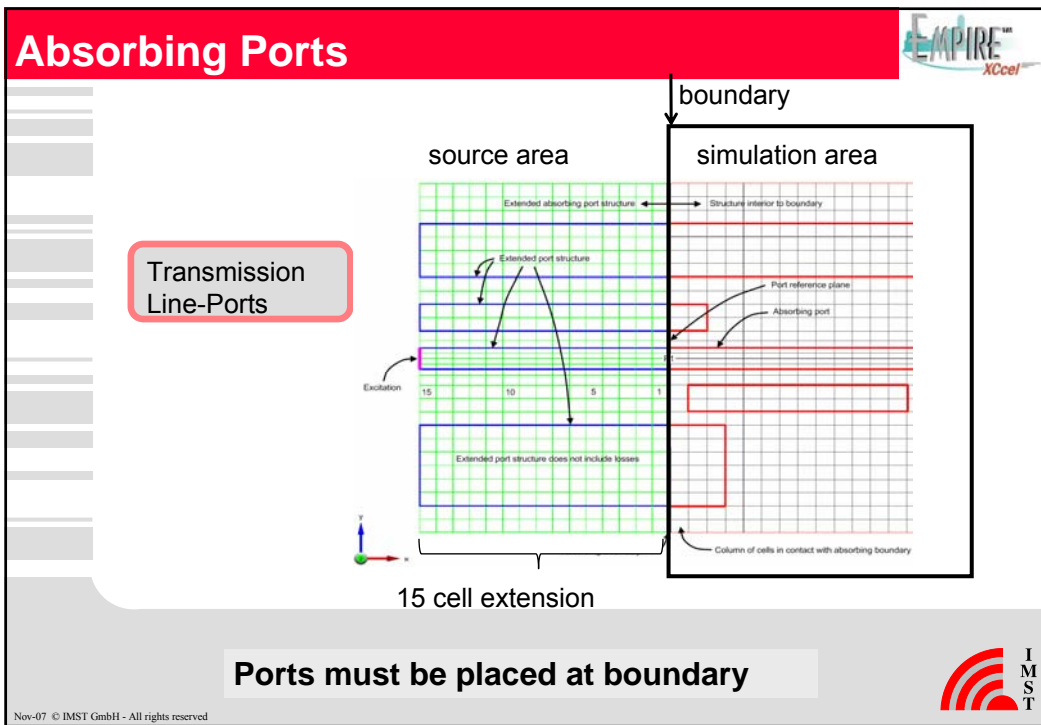
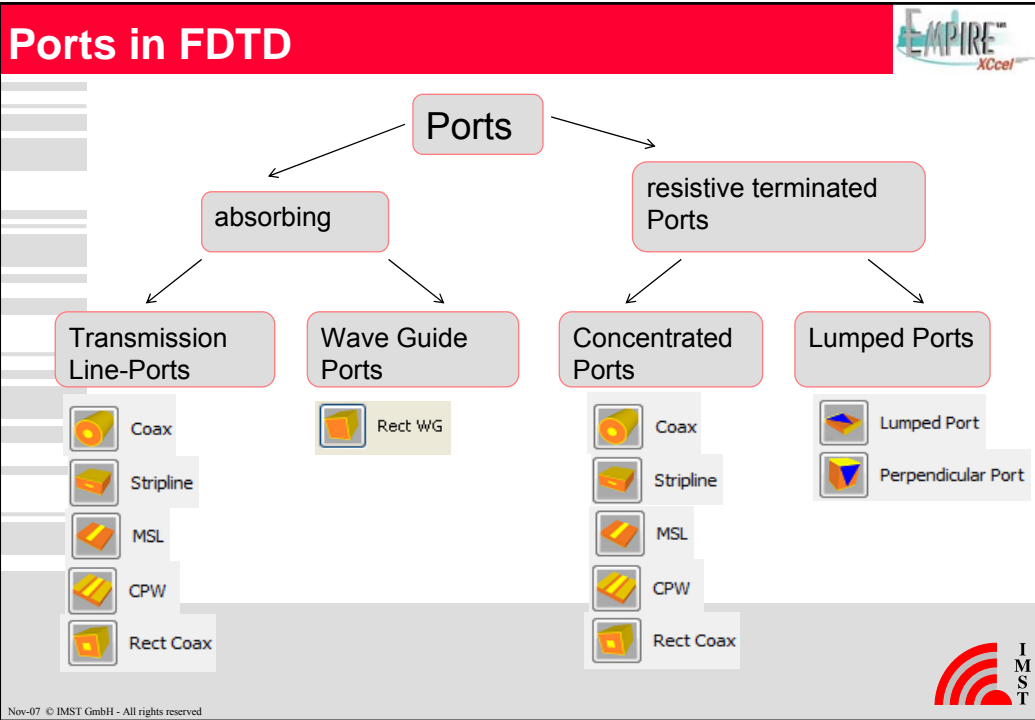
Est. biggest Eigen-Frequency of Equivalent Circuit $\rightarrow \omega_{\max} = \max \sqrt{\frac{1}{C} \sum_L \frac{4}{L}}$

Limitation of time stepping scheme $\rightarrow \Delta_t \leq \frac{2}{\omega_{\max}}$

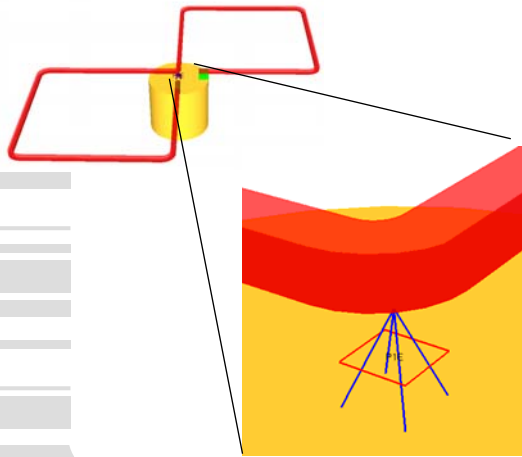
- Improvement Factor 2...20 in strongly graded meshes (e.g. to resolve thin metallisations or nitride sheets)

Nov-07 © IMST GmbH - All rights reserved

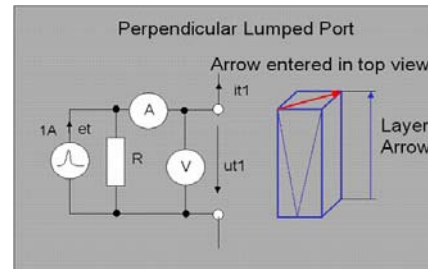




Resistive terminated ports



Perpendicular Port

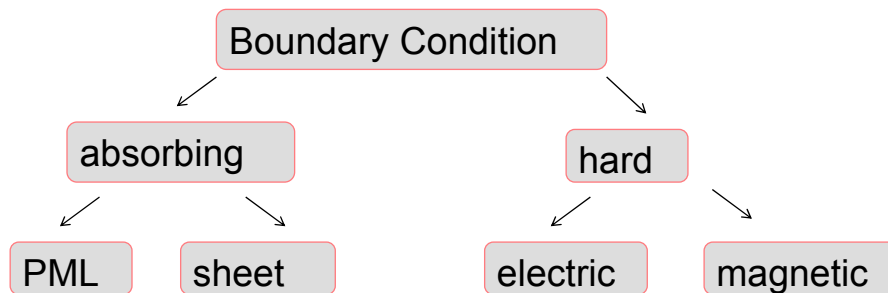


Ports can be placed inside simulation area



Vorlage Nov-07 © IMST GmbH - All rights reserved

Boundaries

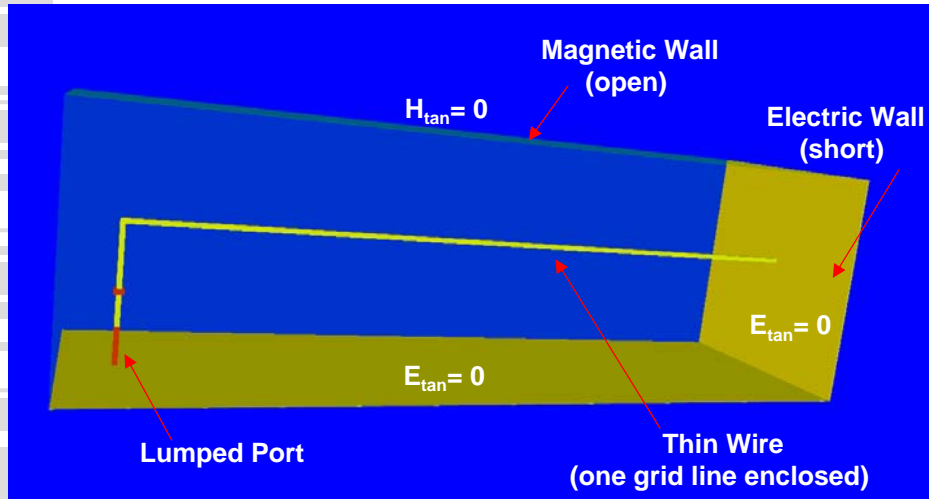


PML (Perfectly matched layer): consists of several lossy layers which are matched to each other

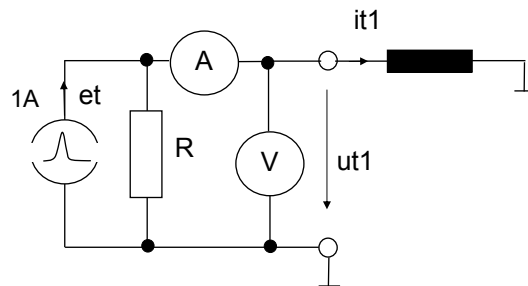
sheet : resistive sheet with $n \times 377 \Omega$ R_{square} , faster than PML, only for perpendicular waves no reflection



Wire example (1)



Wire example (2)



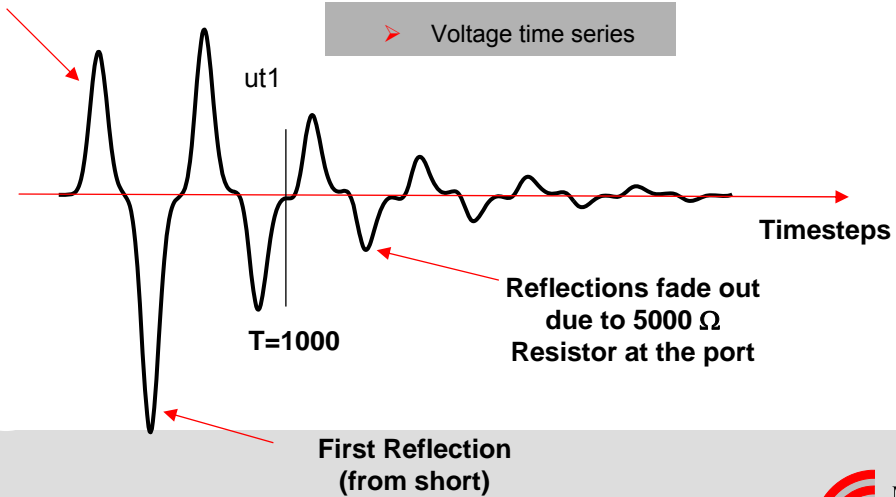
$$et = \exp\left[-\left(\frac{t-t_0}{\tau}\right)^2\right]$$

- Equivalent circuit for port
- Heavyside transformation for separating incident and reflected wave

Wire example (3)



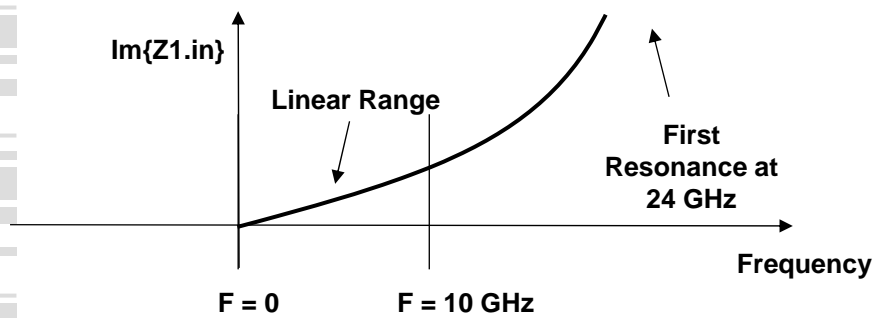
Excitation:
Gaussian Pulse



Wire example (4)

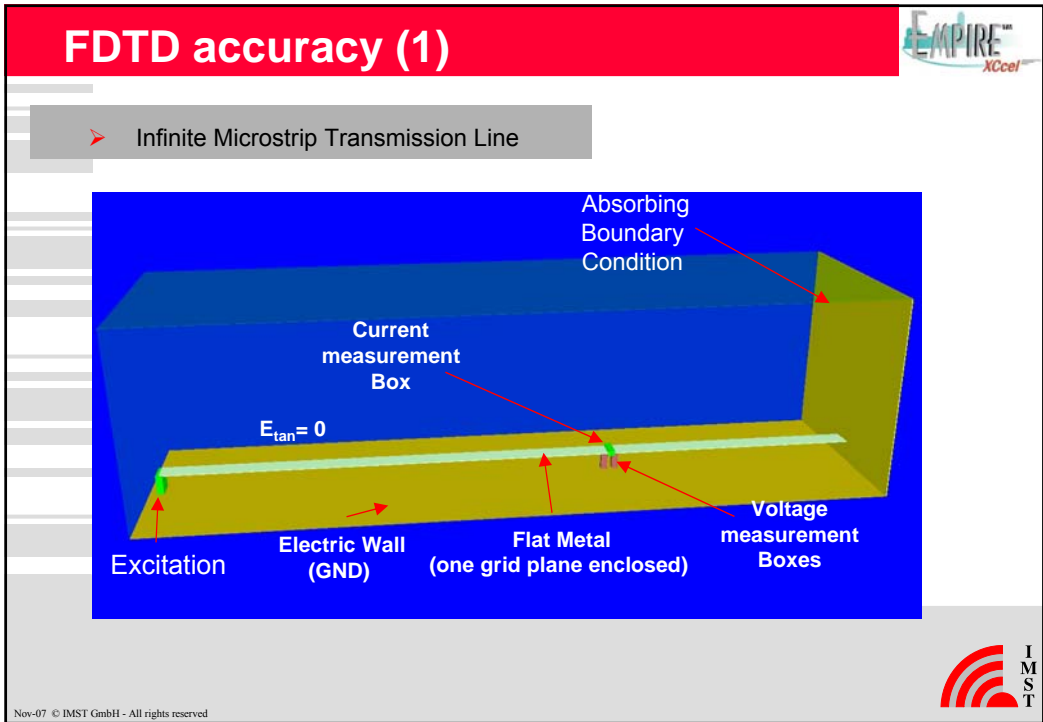
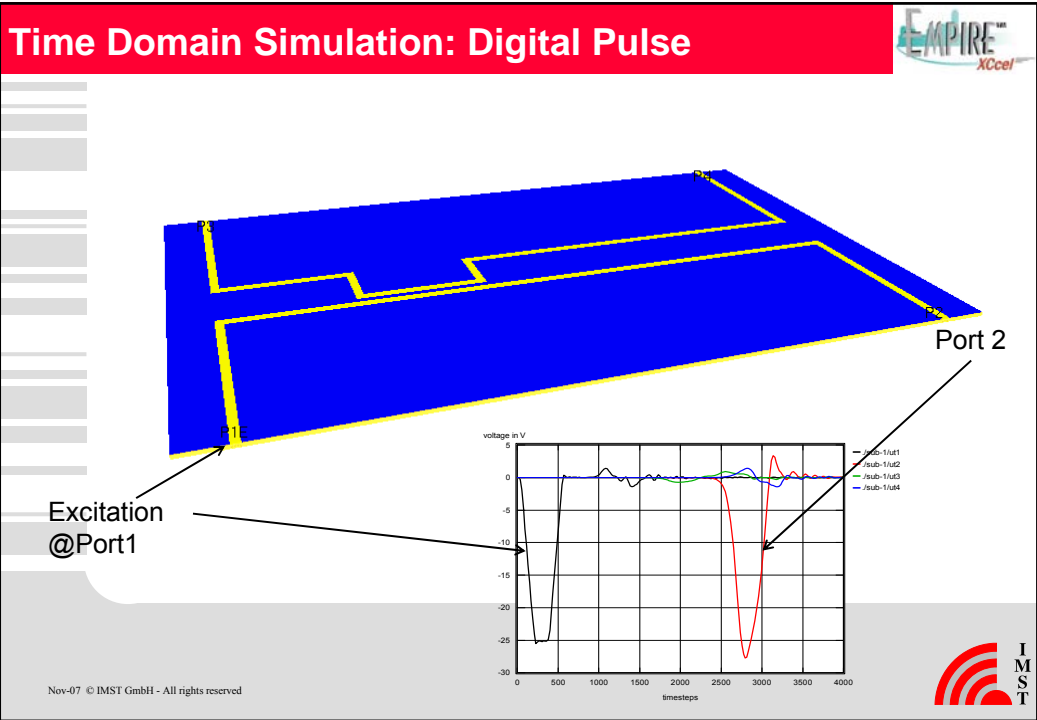


- Discrete Fourier Transformation
- Frequency dependent results: impedances, S-parameters, ...



- Impedance at port
- Inductance $L = \text{Im}\{Z_{1.in}\}/(j\omega)$ for low frequencies (linear range)





FDTD accuracy (2)

- FDTD accuracy is 2nd order, Error $\sim (\Delta_x)^2$
- Flat metallisation makes TEM transmission line parameters only 1st order accurate, Error $\sim \Delta_x$

Cell size

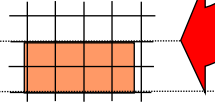
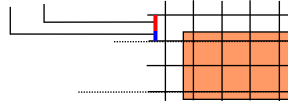
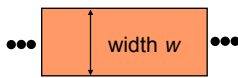
- $1/3 \Delta_x$ Undersizing is another 1st order Error suitable for compensation.

Example:

flat metal line to be sim.

1/3-2/3 Rule mesh generation:

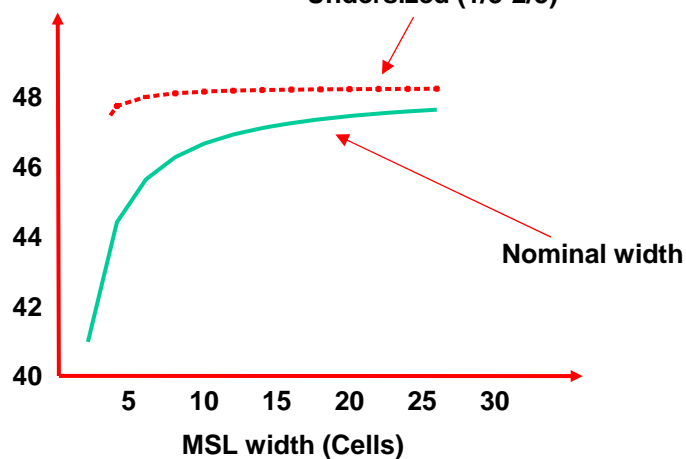
width after mapping on the grid:



FDTD accuracy (3)

Char. Impedance

Undersized (1/3-2/3)



FDTD loss calculation (1)



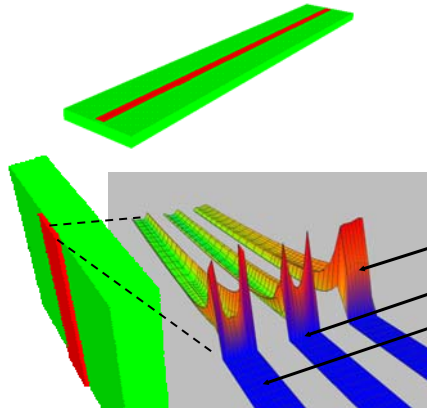
Finite Microstrip Transmission Line

Skin effect:

$$R_{square} = \frac{1}{2\sigma a}$$

$$a(f) = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$h = 635 \mu\text{m}$
 $w = 600 \mu\text{m}$
 $t = 5 \mu\text{m}$
 $\epsilon_r = 10$
 $\ell = 19250 \mu\text{m}$



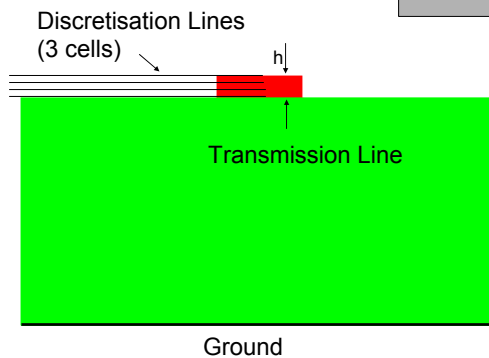
$f = 1 \text{ GHz}$
 $f = 5 \text{ GHz}$
 $f = 25 \text{ GHz}$



FDTD loss calculation (2)



Modelling of the skin effect:



3 options to take into account the skin effect:

1. Resolve Material
 - Fine discretisation. ☹
 - Long simu time ☹
2. Sheet: Narrow band model
 - Resolve with 0 cells (flat) ☺
 - Narrow band ☺
3. Sheet: Broad band model
 - Resolve with 0 or 1 cells (flat) ☺
 - Double sided skin effect ☺
 - Broad band modell ☺



FDTD loss calculation (3)



$$R' l = \frac{l}{\sigma w t} = 0.115 \Omega$$

$$s_{21}(f \rightarrow 0) = -0.02 \text{ dB}$$

Resolved Material:

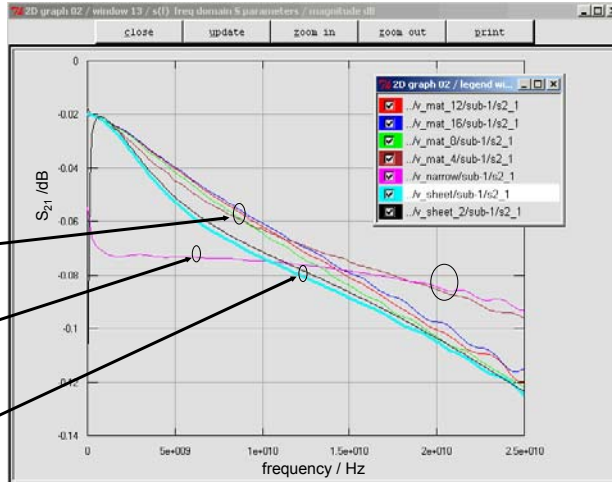
4 cells	200.000 steps
8 cells	400.000 steps
12 cells	600.000 steps
16 cells	800.000 steps

Sheet: Narrow band model:

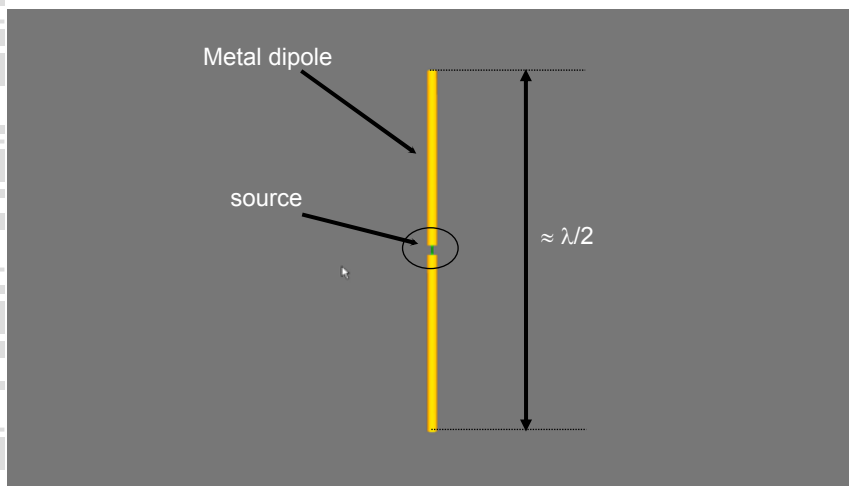
0 cell	3.700 steps
--------	-------------

Sheet: Broad band model:

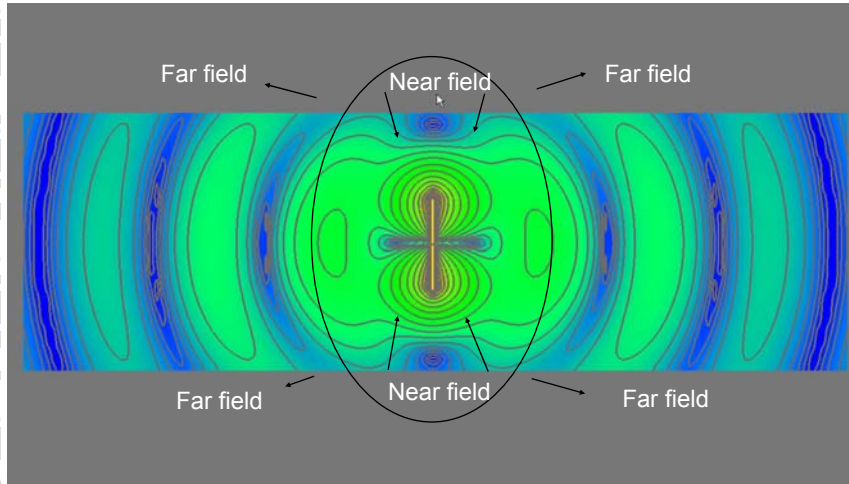
0 cell	3.700 steps (cyan)
1 cell	12.000 steps (black)



Near to far field transformation



Near to far field transformation

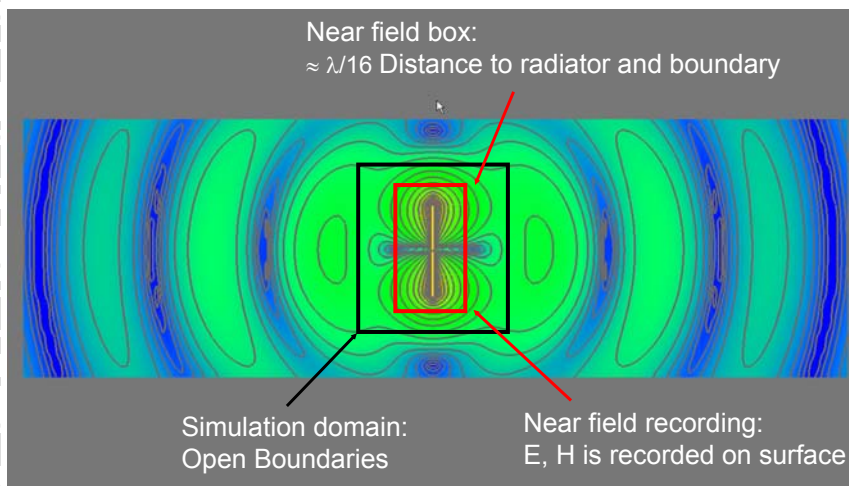


Near field: local resonance (reactive)
Far field: Waves are relieving (radiation)



Nov-07 © IMST GmbH - All rights reserved

Near to far field transformation

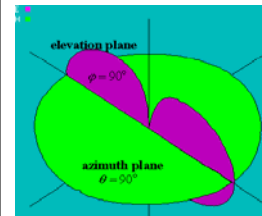
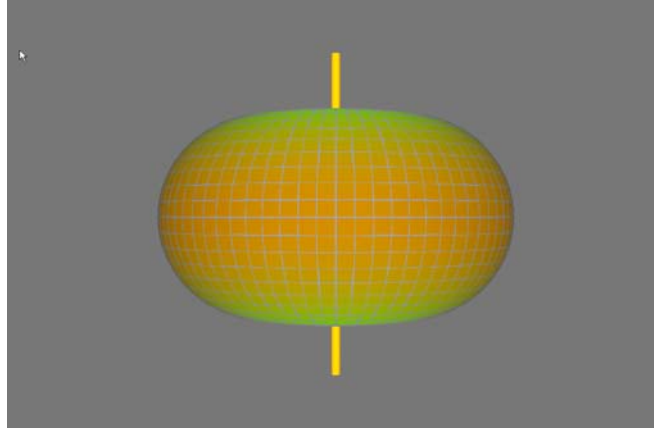


Near field: local resonance (reactive)
Far field: Waves are relieving (radiation)



Nov-07 © IMST GmbH - All rights reserved

Near to far field transformation



Non-uniform radiation: Certain directions are preferred (Directivity= $D(\theta, \varphi)$)



Nov-07 © IMST GmbH - All rights reserved

Speed Optimization



- ✓ **Usage of the new processors (Pentium IV, Athlon 64, Athlon XP, Xeon) 3D calculation extensions (SIMD)**
 - multiple floating point operations each processor cycle
 - usage of multi-level processor cache
- ✓ **Optimized C-code generated for each simulation / structure**
 - only the necessary equations are solved in the specific simulation region
- ✓ **Efficient parallel computing on Multicore CPU's**
 - Innovative usage of multiple core / CPU cache for parallel FDTD calculations
 - simulation time reduced by the factor 10 ... 20

⇒ **Today's performance: ~900 Mcells/s @ Xeon-Architecture**



Nov-07 © IMST GmbH - All rights reserved

Optimized assembler-code for Pentium 4



Precalculated RAM distance

```

movaps 239904(field),xmm0
movaps 240176(field),xmm6
subps  xmm6,xmm0
movaps 119952(field),xmm1
movaps 125664(field),xmm7
subps  xmm1,xmm7
addps  xmm0,xmm7
    
```

$$Ex_k^m = Ex_k^{m-1} + c_k d_k \left(\Delta Hz_k^{n-\frac{1}{2}} + \Delta Hy_k^{n-\frac{1}{2}} \right)$$

$k = \ell, \ell+1, \ell+2, \ell+3$

Sum up 4x4 H-components

```

movaps 48(coeff),xmm3
movaps 48(denorm),xmm4
mulps  xmm4,xmm3
    
```

Denormalize Node Capacities
(less RAM access)

```

mulps  xmm3,xmm7
movaps 359856(field),xmm2
addps  xmm7,xmm2
movaps xmm2,359856(field)
    
```

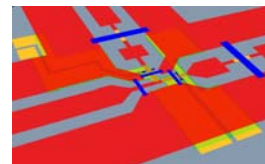
Update 4 E-components



Simulation Speed on multicore CPU's



Computer	Performance
2 x Xeon 5350 2.66 GHz	900e6 cells/s
2 x Xeon 5150 2.66 GHz	500e6 cells/s
1 x Intel Core 2 duo E4500	300e6 cells/s
1 x Xeon 5150 2.66 GHz	245e6 cells/s
AMD 64 X2 4200+ 2.2 GHz	136e6 cells/s
Pentium D 2.8 GHz	190e6 cells/s
P4, 3.4 GHz	102e6 cells/s




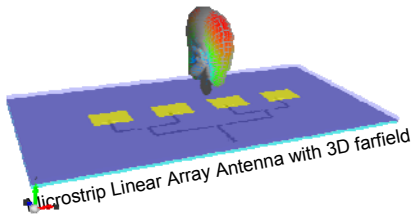
MEMS SPDT switch

- modern 64 bit PC's allow problem sizes up to 48 GB
- ultra fast parallel FDTD simulation on multicore & multi CPU
- PC's reduces simulation time strongly

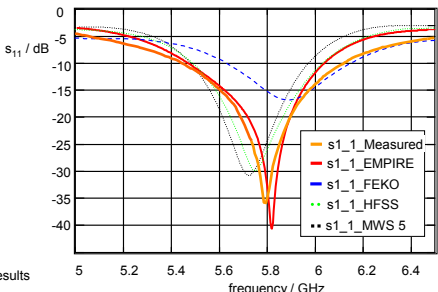


EU-Network of Excellence: ACE – Benchmark






Microstrip Linear Array Antenna with 3D farfield



Results from ACE benchmark comparison:
 The ACE – Network of Excellence is funded within the 6. Frame Programme of The European Union. ACE concentrates on Antenna Theory and Technology. Results of the work are published and disseminated. Please refer for detailed results at <http://www.antennasvce.org> -> Soflab -> Run1)


Software	EMIPRE v. 4.2	CST MWS 5	Ansoft HFSS v. 9	FEKO	MR/FDTD Rennes	IETR	IMELSI IETR	FP-TLM LEAT	IE3D
Total CPU time	10 min	105 min	1879 min	91 min	222 min		780 min	75min	8 min *
Simulation Setup	3D	3D	3D	3D	3D		3D	3D	2.5D *
Type of machine	Desktop PC	Desktop PC	Desktop PC	Desktop PC	Desktop PC		Desktop PC	Parallel CPU WS	Desktop PC
CPU	PIV 3.4 GHz	PIV 1.7 GHz	PIV 2.4 GHz	PIV 3 GHz	AMD 3500+ Athlon		PIV 3 GHz	16 x 1.3 GHz	PIV 3 GHz
Method	FDTD	FITD	FEM	MOM	FDTD		FDTD	TLM	MOM
Used RAM	180 MB		512 MB	143 MB	370 MB		1.3 GB	16 x 466 MB	29 MB

* use of infinite dielectric substrate & infinite metal planes to reduce simulation time




Nov-07 © IMST GmbH - All rights reserved

Conclusions



- Maxwell's Equations discretized in space and time
- EMPIRE yields an improved Stability Criterion for strongly graded meshes
- Fast & Accurate flat metal simulation with 1/3 cell undersizing
- EMPIRE is optimized to efficiently use modern Computers' resources



Nov-07 © IMST GmbH - All rights reserved